

## Original Research Article

# Silanization effect on microtensile bond strength of a self-adhesive luting material to a disilicate-based glass ceramic

Cristina Parise Gré<sup>1</sup>  
Guilherme Carpena Lopes<sup>1</sup>  
Sylvio Monteiro Júnior<sup>1</sup>  
Élito Araújo<sup>1</sup>

### Corresponding author:

Cristina Parise Gré  
Disciplina de Dentística – Sala 138  
Universidade Federal de Santa Catarina – Campus Universitário – Trindade  
CEP 88040-970 – Florianópolis – SC – Brasil  
E-mail: c\_sufi@hotmail.com

<sup>1</sup> Department of Dentistry, Federal University of Santa Catarina – Florianópolis – Santa Catarina – Brazil.

*Received for publication: July 14, 2014. Accepted for publication: February 19, 2015.*

### Keywords:

silane; microtensile;  
lithium disilicate;  
ceramic.

### Abstract

**Introduction:** The rehabilitation of teeth by means of ceramic indirect restorations has been widely performed. Previous studies has shown the effectiveness of silane coupling agents on improving the bond strength of the adhesion of resin cements to ceramics; however, some studies question the use of silane. **Objective:** To evaluate the effect of silane application on the microtensile bond strength of an auto-adhesive luting material to a lithium disilicate glass-ceramic. **Material and methods:** Two blocks (9x11x4mm) of lithium disilicate glass-ceramic had one of their surfaces polished (# 220, 360, 600 grit silicon-carbide abrasive papers) and cleaned ultrasonically. The ceramic blocks were then divided into two groups according to the surface treatment: G1 (control group): etched with 10% hydrofluoric acid for 20s and silane coated; G2: etched with 10% hydrofluoric acid for 20s. After building two blocks of composite resin (Filtek Z350) with the same dimensions of the ceramic blocks, the self-adhesive resin cement (SpeedCEM) was applied directly to the ceramic surface and the resin block was seated on the cement. After storage (24h, 37°C), the ceramic-cement-composite blocks were cut with an Isomet low-speed diamond saw machine producing sticks, which were loaded to failure at a crosshead speed of 0.5 mm/min. The type of fracture was analyzed under an optical microscope. The results were statistically analyzed using the Student t test. **Results:** The mean microtensile and standard deviations in megaPascals were:

G1 = 21.32 ( $\pm$  4.36) and G2 = 16.55 ( $\pm$  4.92). Statistical analysis showed that the bond strength was not significantly affected by the surface treatment with silane. Most of the fractures occurred within the adhesion zone. **Conclusion:** The application of silane had no significant effect on the bond strength between lithium disilicate glass-ceramic and self-adhesive resin cement.

## Introduction

The rehabilitation of teeth by means of indirect restorations in ceramic has been increasingly performed [1, 18]. A growing number of ceramic systems cemented by adhesive technique are available for clinical use and many studies have reported clinical long-term success of this restoration type [4].

The clinical success of ceramic restorations cemented by the adhesive technique is highly dependent on a stable and durable adhesive bond [23]. Such union is dependent on the surface energy and the degree of wetting of the adhesive by the adhesive [9]. The adhesion between dental ceramics and composite resins is the result of physical-chemical interaction through the interface between the adhesive and the substrate [9], which can be achieved by two mechanisms: 1) micromechanical adhesion by use of hydrofluoric acid and/or sandblasting; and 2) chemical adhesion through a silane coupling agent [13]. The hydrofluoric acid removes the glass matrix and the second crystalline phase, creating irregularities on IPS e.max lithium disilicate crystals, allowing mechanics adhesion to resin composites [5]. The silane coupling agent has bifunctional characteristics promoting chemical interaction between the silica layer of the vitreous phase of ceramics and the methacrylate groups of resins through siloxane bonds [19].

The etching of the surface and silane application increases the surface energy and the degree of wetting of the ceramic surface [2, 6].

Silane coupling agents are used since 1949 to improve the union of adhesives (of organic nature), ceramics and metals, but only in 1977 Eames and colleagues suggested the use of silanes in dentistry [12].

Previous studies have reported the effectiveness of the silane coupling agent to increase the bond strength between composite resins and ceramics [10, 17] and between resin cements and ceramics [6, 16, 25]; however, some studies [9, 11, 20, 27] doubt on the use of silane. Authors state that the application of silane had no significant effect on

the bond strength between ceramics and resin cements [9, 11, 27].

Such materials using adhesive system through total etching or self-etching agents, followed by applying a composite resin of low viscosity [7], which makes their use complicated and may interfere with adhesion. Adhesive systems that combine adhesive and cement in a single application have been introduced to the market [11]. The self-adhesive resin cement tested in this study contains, according to the manufacturer, adhesive monomers formed by a long methacrylate chain with a phosphoric acid group able to establish chemical bonds to the tooth structure and to ceramic surfaces. Thus, additional bonding agents are not required [14].

Recently introduced in the market, the glass-ceramic-based lithium disilicate IPS e.max Press (Ivoclar Vivadent, Schaan, Liechtenstein) offers excellent esthetics and features, according to the manufacturer, high flexural strength values ( $\pm$  400 MPa). The manufacturer recommends the use of hydrofluoric acid associated with a conventional silane agent for bonding procedures due to the glass phase present in these ceramics [15].

This study evaluated the influence of silane coupling agent application on microtensile bond strength of self-adhesive resin cement to lithium disilicate reinforced glass ceramic, the IPS e.max system. The tested null hypothesis is that there was no influence of silane coupling agent application on the bond strength of self-adhesive resin cement to lithium disilicate-based ceramics.

## Material and methods

Two blocks, each measuring 11 mm long x 9 mm in width x 4 mm in height, were made of wax casting, included in coating (IPS e.max Press), and the ceramic was infiltrated under pressure in EP 500 special oven. The obtained ceramic blocks were sandblasted with aluminum oxide to remove the coating.

**Table I** - Materials used and their compositions

Material	Composition	Manufacturer	Batch
IPS e.max Press tablets	SiO <sub>2</sub> ; Li <sub>2</sub> O; K <sub>2</sub> O; MgO; ZnO; Al <sub>2</sub> O <sub>3</sub> ; P <sub>2</sub> O <sub>5</sub> ; other oxides	Ivoclar Vivadent, Schaan, Liechtenstein	R37944
Silane Monobond S	Alcoholic solution of silane methacrylate; 1% 3-methacryloxypropyltrimethoxysilane; 99% water and ethanol; acetic acid	Ivoclar Vivadent, Schaan, Liechtenstein	P70737
Self-etch resin cement SpeedCem	Dimethacrylates; acidic monomers; barium glass; ytterbium trifluoride; copolymer and silicon dioxide; initiators; stabilizers	Ivoclar Vivadent, Schaan, Liechtenstein	S33619
Resin Composite Filtek Z350	BIS-GMA; BIS-EMA; UDMA; TEGDMA; filler particles	3M ESPE, Saint Paul, MN, United States	N187685

For standardization, a surface of each ceramic block was polished, refrigerated, in a polishing machine (Panambra, SP, Brasil), with sandpaper (Acqua Flex-Norton, SP, Brasil) e in descending order of granulation - 220, 360 600 - cleaned in ultrasonic bath with distilled water for 5 min and dried with compressed air. The blocks were then divided into two groups according to the surface treatment they were submitted to:

- Group 1 (control): etching with 10% hydrofluoric acid (Condac porcelana, FGM, Joinville, SC, Brazil) for 20 s, rinsing with compressed air / water jet for 30 s, air drying for 30 s, followed by silane application (Monobond S-Ivoclar Vivadent, Schaan, Liechtenstein). After 60 s, silane reaction time, the surfaces were dried with compressed air jet for 30 s;
- Group 2: etching with 10% hydrofluoric acid for 20 sec, rinsing with compressed air/water for 30 s, air drying for 30 s without the subsequent application of silane.

Following, two composite resin blocks (Filtek Z350, shade A2, 3M ESPE, St. Paul, MN, USA) with the same dimensions of the ceramic blocks were made. Therefore, each ceramic block was submitted to impression with polymerized addition silicon (Virtual, Ivoclar Vivadent; Schaan, Liechtenstein) to obtain a matrix. The composite resin was inserted in the array at 2 mm increments, and each increment was light-cured for 20 s by a light-curing unit (Translux Power Blue-Hareaus Kulzer GmbH-Hanau, Germany) with light intensity (750mW/cm<sup>2</sup>) measured prior to its use by a radiometer.

After the surface treatment of ceramic and the resin blocks already ready, the self-adhesive

resin cement SpeedCem (Ivoclar Vivadent; Schaan, Liechtenstein) was applied directly on the ceramic surface. The resin block was sitting onto the cement and, to standardize the load cementing of the ceramic-polymer-cement assembly, at the moment of the resin block sitting, a cementing device with a load of 1 kg was used.

After 24 h in distilled water at 37°C, the specimens were placed in the cutting machine (ISOMET 1000, Buehler, Lake Bluff, IL, USA) for manufacturing the sticks for the microtensile test. The blocks were sectioned at ceramic-resin direction, resulting in sticks with cross-sectional area of approximately 0.8 mm<sup>2</sup>. The width and thickness of the sticks were measured with a digital caliper (KingTools, São Paulo, SP, Brazil) with a precision of 0.01 mm, and 25 specimens of each group were randomized to be submitted to microtensile test.

The sticks were individually glued at their ends to a special microtensile device (Geraldeli device for microtensile) adapted to a universal testing machine (Instron, model 4444, Instron Corp. Canton, MA, USA), and microtensile test was performed at a crosshead speed of 0.5 mm/min until the fracture. The type of fracture was assessed by optical microscope (Olympus BX 60, Olympus Optical do Brasil Ltd., São Paulo, SP, Brazil) at x20 magnification. The fractures were classified as adhesive (as occurred in the adhesive interface), cohesive in ceramic (when occurring in the ceramic substrate), cohesive in resin (when occurring in composite resin) and mixed (when involved more than one substrate). The microtensile bond strength was calculated and the values were expressed in MPa. The results were evaluated through Student's t-test with 0.05 significance level.

## Results

The Student t test showed no significant difference between the groups tested ( $p > 0.05$ ). The microtensile bond strength was not significantly affected by silane application to the ceramic surface.

The mean bond strength (MPa) and the standard deviation found in G1 and G2 were: G1 = 21.32

( $\pm 4.36$ ) and G2 = 16.55 ( $\pm 4.92$ ) (table II). It was found a value of  $p = 0.787$  and, therefore the null hypothesis was accepted. The pre-test failures were 8.33% for G1 and 6.89% for G2; however these failures were not considered for determining the mean and statistical analysis.

Most fractures occurred in the adhesive interface between the ceramic and resin cement, in both groups (table III).

**Table II** - Descriptive statistics of the microtensile bond strength test (it will be present the values of n, mean, standard deviation and confidence intervals for a 95% confidence level)

Group	n	Mean (MPa)	Standard deviation (MPa)	MPa -95%	MPa + 95%	Variation coefficient
G1	25	21.32	4.36	19.66	22.98	20.45%
G2	25	16.55	4.92	14.60	18.50	29.72%

**Table III** - Distribution of the types of failures of the specimens after microtensile test

Group	n	Adhesive failure at ceramic/cement interface	Adhesive failure at resin/cement interface	Adhesive failure at resin	Adhesive failure at ceramic
G1	25	21	2	2	0
G2	25	22	2	0	1

## Discussion

Several factors are relevant to the success of ceramic restorations cemented adhesively, because it is essential to create a stable and lasting adhesion. Several methods are available to evaluate the bond strength. One of the tests more used is the shear bond strength test, which often produces cohesive fractures in substrate, far from the adhesive area due to poor stress distribution at the testing time, generating erroneous results [8, 23].

In this study we used the microtensile test, recommended by Sano and colleagues [24], but without additional wear for preparing the hourglass shape specimens [26], seeking a better stress distribution at the adhesive interface. The adhesive area of the specimens prepared in this study was approximately 0.8 mm<sup>2</sup>, allowing a more uniform stress distribution at the moment of load application, and prevailing failures in the adhesive interface.

The results of this study showed that the application of silane coupling agent on the ceramic surface did not influence the microtensile bond strength values of the self-adhesive resin cement to glass ceramic.

The silane application on the surface of glass ceramics after etching with hydrofluoric acid is an established surface treatment in the literature,

for generating good bond strength values [3, 10]. Due to its bifunctional characteristics, the silane application to the etched ceramic surface improves the bond of ceramics to resin materials since the silane coupling agent is able to bond, through siloxane bonds, the silica present in ceramic surface to the resin organic matrix [19].

Differently from studies that prove the effectiveness of silane coupling agent in improving the bond strength of resin cements to ceramics [6, 21, 25], in this study, the application of silane after the ceramic acid etching did not influence on the bond strength of the self-adhesive resin cement to lithium disilicate based ceramics. This result suggests that a chemical reaction between the self-adhesive resin cement and glass ceramic occurred, probably based on an interaction between the phosphoric acid group present in the resin cement and ceramic surface oxides, making unnecessary the silane application in cases which this chemical bond is effective [20].

This study agrees with previous and studies questioning the use of silane in previously conditioned ceramic surface. Sorensen and colleagues [27] reported no difference in the amounts of shear bond strength of ceramic to resin cements between silanized and non-silanized groups. For

Della Bona *et al.* [9], surface treatment with silane coupling agent decreased the energy surface of the ceramic, which reduced the degree of wetting of the surface by the resin cement. According to Oliveira and colleagues [20], silanization did not improved shear bond strength values of self-adhesive resin cements to glass fiber posts because the post's surface became non-polar, which would impair the wetting of the post surface by the cement. Dos Santos *et al.* [11] also reported no difference in bond strength values of composite resin to resin self-adhesive cement between silanized and non-silanized groups.

As mentioned above, the silanization may be unnecessary when effective chemical bond of the self-adhesive resin cement to the glass phase of the ceramic occurs. A possible explanation for these results is that the silane layer may restrict the interaction between the acid groups present in phosphoric acid groups from the self-adhesive cement and the glass ceramic layer [20].

Studies show that the conditioning of the ceramic by hydrofluoric acid creates micro retentions that cause satisfactory adhesion results of resin cement to ceramics conditioned by acid [6, 28]. Therefore, both groups herein tested underwent etching by hydrofluoric acid.

## Conclusion

The application of silane coupling agent on a ceramic surface previously conditioned by hydrofluoric acid did not increase the microtensile bond strength of self-adhesive resin cement to a lithium disilicate-based glass ceramic.

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